Industrial Compressor Impeller Strength Evaluation

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Abstract: Impellers are for our company subject of experimental stress analysis, because are the most important parts of the compressors. All information about impellers are key to the development of our company, therefore is testing of impellers our integral part.

Keywords: Impeller; Over-Spin Test; Non Destructive Testing.

1 Introduction

An impeller is a key structural part of an industrial turbo-compressor. The machine parameters are given namely by a rotor speed. For the high-sophisticated product, an effort to speed increase up to material limit is emphasized. Impeller behavior is studied from the mechanical point of view and appropriate analysis methods and evaluation criteria are submitted.

2 Standards

2.1 Product

Impeller design, manufacture and quality assurance are described in product standards. API 617 or ISO 10439-1 are the best known specifications. The over-spin test of each specimen is often demanded. This "virgin" load exceeds the operation one by 15 to 21 %. Except traditional demonstration of object integrity, over-load causes plastic deformations in the critical areas.

2.2 Material

Impellers are made from steel or titanium alloy. Other materials, such as aluminium, may be used in specific applications. Material limits are listed in relevant standard. A minimal strength is referred to chosen heat treatment. It is practical to use international standards for communication between designer and supplier, e.g. EN 10250-4 for steel forgings.

2.3 Low-Speed Balancing

For better properties of impellers and balanced rotation of train, the impellers are balanced. The impellers are usually balanced by taking away some material from the impellers. For this process of determination the best properties of impellers, a balancing machine is used, Fig. 1.

3 Theory

3.1 Stress Distribution

An impeller load comes from mainly centrifugal movement. Rotating disc may burst. However blading causes stress concentration in the blade to shroud or blade to hub joins. Because of mechanical design is driven by flow channel optimized for aerodynamics, there are several isolated critical areas.



Fig. 1: Low-speed balancing machine.

3.2 Plastic Deformation

A plastic part of stress-strain curve is exploited in the course of initial over-spin test. Cyclic deformation should be considered.

Example of test report balancing, overspeed testing and dimensional check of impellers is shows in attachment.

4 Methods

4.1 Stress Analysis

Impeller geometry is analyzed via finite element method. High level stress areas are optimized and maximum rotor speed is estimated.

4.2 Plastic Deformation

At the first step which is "over-spin" (once in a lifetime), the material may be partially plastic deformed (maximum half of a cross-section). The next steps plastic deformation has to remain the same (linear).

4.3 Over-Spin Test

Each manufactured specimen is tested in laboratory. A non-destructive testing is performed consequently. Sustaining of the over-spin gives potential to be operated without failure.

Example you can see in attachment.

5 Best Practice

5.1 Design Criterion

In the course of impeller design, the geometry is optimized from the thermodynamic as well as mechanical point of view. Stress analysis during design session has 2 purposes:

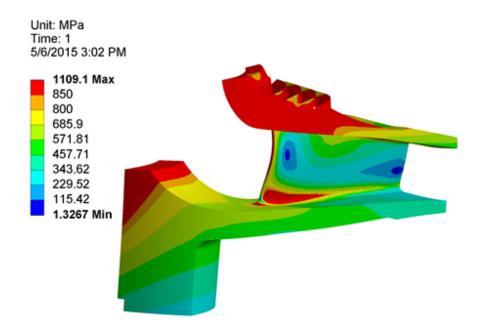


Fig. 2: Final element analysis stress von-Mises.

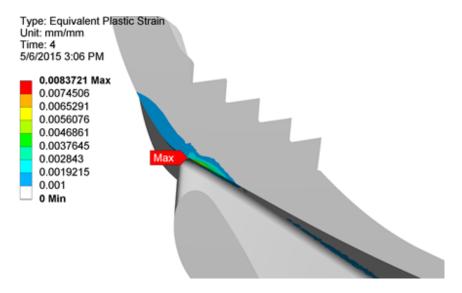


Fig. 3: Final element analysis equivalent plastic strain deformation (cross-section).

- critical areas identification and geometry optimization,
- impeller strength limit estimation.

Sufficient strength of the given specimen shall be experimentally verified prior machine operation because of safety as well as economic reasons. An appropriate criterion should be developed. It is proposed to evaluate

- maximal plasticity of material in critical area,
- plastic zone dimension related to full cross-section (max. half of the cross-section).

5.2 Experiment Evaluation

In the course of experimental session, the object carries an overload. The experiment evaluation provides us with 2 important QA items:

- maximal plasticity of material in critical area,
- plastic zone dimension related to full cross-section (max. half of the cross-section).

The first item is evaluated by the non-destructive testing. Traditional methods, e.g. liquid penetrants or magnetic particle, are used to be applied. For the second one, an appropriate criterion should be developed. Object strength evaluation is based on stress analysis. A plastic deformation after repeated application of the spin load is evaluated.



Fig. 4: Over-spin testing.

6 Conclusion

An industrial compressor impeller is subject of experimental stress analysis. Even a local material static strength exceeding is indicated via NDT or via loss of object integrity. Plastic deformation is evaluated via outside measurable dimension. Cyclic deformation curve is used for operation safety guarantee confirming numerical simulation results.

7 Attachment

	VÁŽENÍ, ODSTŘEDĚ ALANCING, OVERSP							1	
ISO 9001 LC-C (Certificative)		CHOZÍ ROVIN KOVKU NA N FERENCE PLA MOING NUMBE	OSNEM NE - BEC	KOTOUCI SINNIS OF THE	4		ØD2		
Číslo výkresu kola	DC-11826-P-00717			Hmotnost kola			25.4 kg		
impeller draw. No. Číslo výkovku nosného kotouče		Impeller mass Číslo výkovku krycího kotouče		20,4 10		kg			
Hub disk forging No. VYVÁŽENÍ KOLA	Shroud disk forging Maintenance Partners – 101J-HD STA						•		
IMPELLER BALANCING	Maintena	nce Partne	rs – 1	01J-HD STAC	GE 1 IM	PELLER	\$		
Typ vyvažovaciho stroje	SCHENCK H3	Vjr. č. vyvažovaciho stroje Balanc. machine manufac. No.		AHE 1195					
Balancing machine type Přípustná nevyváženost		-		c. machine manu tovací otáčky	fac. No.	- '	And Tibe		
dle ISO 1940 G 2,5 e=1,98 Permissible unbalance	50,2	gmm		cing speed			340	1/min	
Počáteční nevyváženost R=210mm Initial unbalance	1575	gmm	Provedi Petr Hol						
Zbytková nevyváženost Residual unbalance	14,7	gmm	Datum 22.4.2015			Podpi Signa			
ROZMĚROVÁ KONTROLA OB DIMENSIONAL CHECK OF THE IMPEL		Maintenan		rtners – 101J	HD ST			.ER	
Mêfené misto									
Measurement point	1	2		3		4 5			
Připustné trvalé deformace Permissible pernament deformation	0,000 09. D2 min. 0,03 mm				0,000 11. D2 min. 0,04 mm				
Průměry před odstředěním Diameters before overspeed test	305,030	153,5	00	152,310	454,070		45	454,030	
Průměry před odstředěním Diameters before overspeed test	305,050	153,50	00	152,310	454	,090	454,050		
Průměry po odstředění Diameters after overspeed test	305,050	153,50	00 152,310		454	4,080 454,050		4,050	
Průměry po odstředění Diameters after overspeed test B	305,050	153,500		152,310	454	1,110	454,070		
Teplota měřeného kola před odstředěr Temperature of measured impeller ber		*C Provedi: Performed:							
Teplota měřeného kola po odstředění		to Datum: 0			Podpis, razilko				
Temperature of measured impeller after			Date:	a - 101J-HD STAGE 1 IMPELLER				nρ	
ODSTŘEDĚNÍ KOLA OVERSPEED TEST OF THE IMPEL		ice Partne	rs – 1	01J-HD STAG	SE 1 IM	PELLER	1		
Typ odt/ed/ovaciho stroje Overspeed machine type	B4 P		Výr. č. odtřeďovacího stroj Overspeed machine manu			ABF 0009			
Odsředovací otáčky Overspeed	13 869	1/min	Prove	Date	r Holý				
Doba Duration	1	min	Datam 22.4.2015 Po				is ture		
Hesio Code Maintenance Partners	Zakázkové číslo Order No.	akázkové číslo V4E44E				POČ OrderConf. No.			
Příloha – průběh odstřeďování kola Appendix – course of overspeed					Typ Type -				
Schváll : Approved : Datum :	Výsledek měření 🕽 Result of measurement	of acceptable non-acceptable arement				Číslo: Number:			
Data :	Podpis, razilko Signature, stamp				MP-P	ZZ-00	1A		

Fig. 5: Test report balancing, overspeed testing and dimensional check of impeller 1/2.

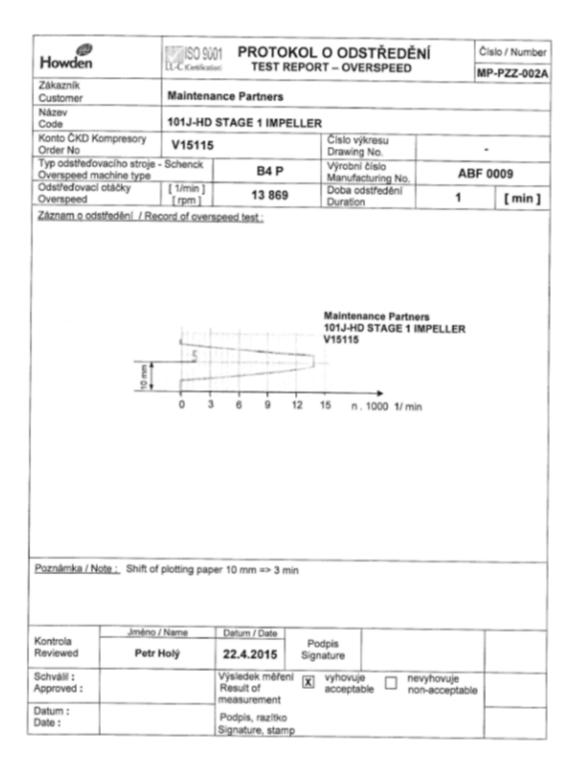


Fig. 6: Test report balancing, overspeed testing and dimensional check of impeller 2/2.