

PROBABILISTIC SOLUTION OF HARD ROCK DISINTEGRATION PROCESS

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Abstract: This paper focuses on a numerical analysis of the hard rock (platinum ore) disintegration process. The bit moves into the ore (i.e. mechanical contact with friction) and subsequently disintegrates it. The disintegration (i.e. stress-strain relationship, reaction forces and fracture of the ore etc.) is solved via the FEM in combination with SBRA (Simulation-Based Reliability Assessment) method (i.e. Monte Carlo simulations). The ore is disintegrated by deactivating the finite elements which satisfy the fracture condition. Material of the ore (i.e. yield stress, fracture limit, etc.), is given by bounded histograms (i.e. stochastic inputs). The results are compared with experiments. Application of the SBRA method in this area is a new and innovative trend. However, it takes a long time to solve this problem (due to material and structural nonlinearities, the large number of elements, many Monte Carlo simulations, etc.). Hence, parallel computers were used to handle the large computational needs. Finally, the probabilistic reliability assessment is proposed.

1. Introduction



Figure 1: Typical Example of Mechanical Interaction between Bits and Hard Rock (Ore Disintegration Process).

stochastic approach (i.e. Simulation-Based Reliability Assessment Method) in combination with FEM is applied.

Scientific and technical developments (in all areas of world-wide industry) are affected by the growing demand for basic raw materials and energy. The provision of sufficient quantities of raw materials and energy for the processing industry is the main limiting factor of further development. It is therefore very important to understand the ore disintegration process, including an analysis of the bit (i.e. excavation tool) used in mining operations. The main focus is on modelling of the mechanical contact between the bit and the platinum ore and its evaluation (i.e. practical application in the mining technology), see Figure 1. However, material properties of the ore (as known from nature) have a large stochastic variability. Hence, the

2. Finite Element Model of the Ore Disintegration Process

FEM (i.e. MSC.Marc/Mentat software, see references [1], [2] and [3]) was used in modelling the ore disintegration process.

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Figure 2 shows the basic scheme (quasi-static loading, plain strain formulation, mechanical contact with friction between the bit and platinum ore, boundary conditions, etc.). The bit moves into the ore with the prescribed time dependent function and subsequently disintegrates it. When the bit moves into the ore (i.e. a mechanical contact occurs between the bit and the ore) the stresses σ_{HMH} (i.e. the equivalent von Mises stresses) in the ore increase.

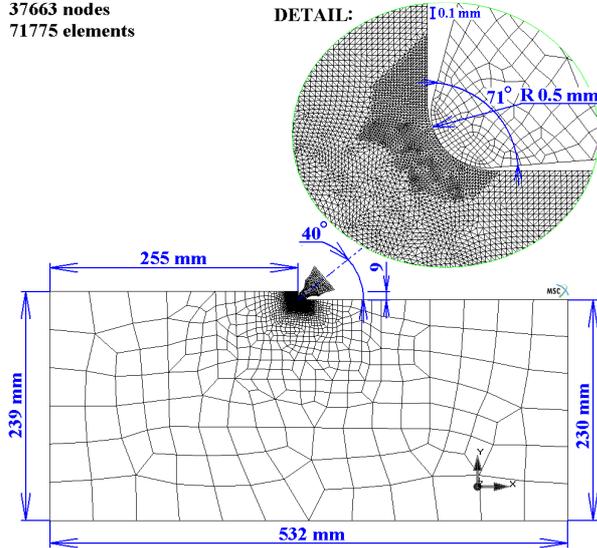


Figure 2: Finite Element Model and its Dimensions.

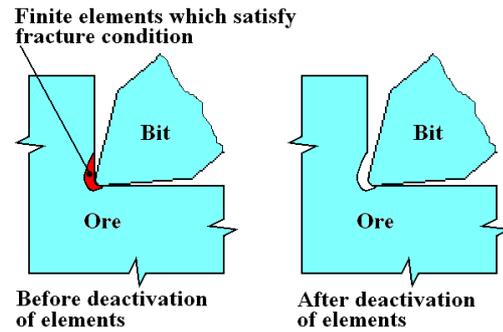


Figure 3: Disintegration of a Part of the Ore.

When the situation $\sigma_{HMH} \geq R_m$ occurs (i.e. the equivalent stress is greater than the tensile strength) in some elements of the ore, then these elements break off (i.e. these elements are dead). Hence, a part of the ore disintegrates. In MSC.Marc/Mentat software, this is done by deactivating the elements that satisfy the condition $\sigma_{HMH} \geq R_m$. This deactivation of the elements was performed in every 5th step of the solution, see Figure 3.

For further information see references [1], [2] and [3].

3. Probabilistic Inputs and SBRA (Simulation-Based Reliability Assessment) Method

A deterministic approach (i.e. all types of loading, dimensions and material parameters etc. are constant) provides an older but simple way to simulate mechanical systems. However, a deterministic approach cannot truly include the variability of all inputs (i.e. variability of material properties of the ore), because nature and the world are stochastic. Solution of the ore disintegration process via deterministic approach (i.e. basic simple solution) is shown in reference [3]. However, this problem is solved via probabilistic approaches which are based on statistics.

Let us consider the "Simulation-Based Reliability Assessment" (SBRA) Method, a probabilistic direct Monte Carlo approach, in which all inputs are given by bounded (truncated) histograms. Bounded histograms include the real variability of the inputs. Application of the SBRA method (based on Monte Carlo simulations) is a modern and innovative trend in mechanics, for example see references [4].

The material properties (i.e. isotropic and homogeneous materials) of the whole system are described in Figure 4, where E is Young's modulus of elasticity and μ is Poisson's ratio.

The bit is made of sintered carbide (sharp edge) and steel. Stochastic influences of material parameters of the bit can be neglected.

Sintered Carbide ($E = 600000$ MPa, $\mu = 0.22$) - constant value
 Steel ($E = 210000$ MPa, $\mu = 0.31$) - constant values
 Ore (E, μ, R_p, R_m are given by bounded histograms)
 - stochastic values

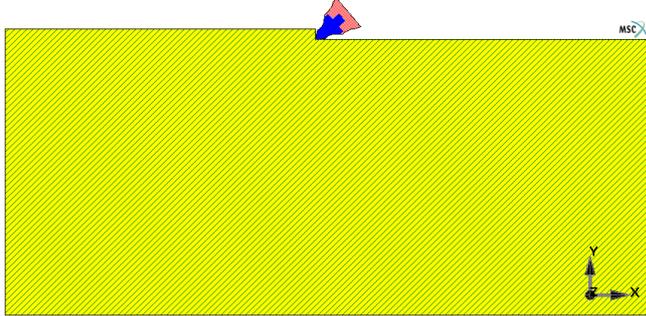


Figure 4: Material Properties (Whole Model).

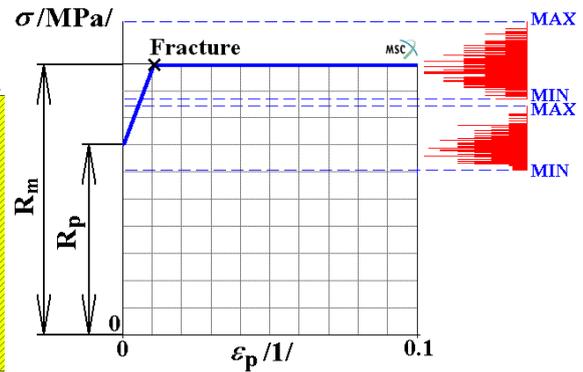


Figure 5: Stochastic Material Properties of the Ore (Stress σ vs. Plastic Strain ϵ_p).

The ore material is elasto-plastic with isotropic hardening rule. The plastic properties are described by yield stress $R_p = 9.946^{+1.722}_{-0.911}$ MPa and fracture stress $R_m = 12.661^{+0.925}_{-0.650}$ MPa, which are given by bounded histograms, see Figure 5.

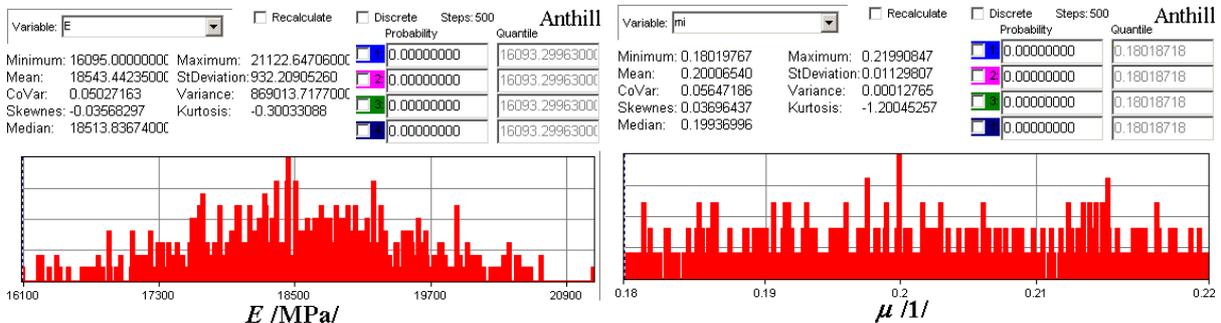


Figure 6: Stochastic Inputs for the Material of the Ore (Histograms of Young's Modulus and Poisson's Ratio).

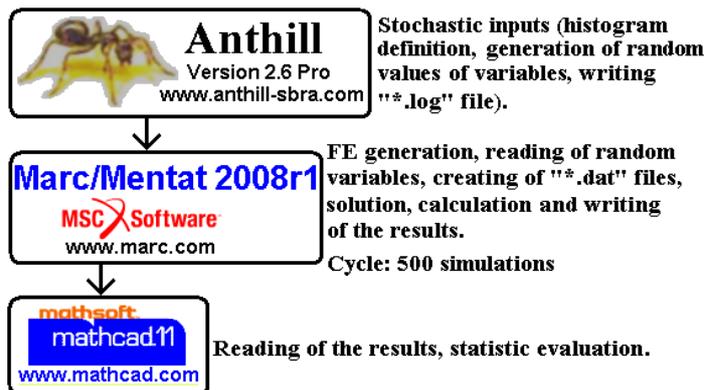


Figure 7: Computational Procedure - Application of the SBRA Method and FEM (Solution of the Ore Disintegration Process).

The elastic properties of the ore are described by Hooke's law in the histograms

($E = 18513.8^{+2608.8}_{-2418.8}$ MPa and $\mu = 0.199^{+0.021}_{-0.019}$), see Figures 6.

The results (acquired by SBRA method in combination with FEM) were subsequently statistically evaluated, as shown in Figure 7. Anthill, MSC.Marc/Mentat and Mathcad software were used.

Because of the material non-linearities, the mechanical contacts

with friction, the large number of elements, many iteration steps, and the choice of 500 Monte Carlo simulations, four parallel computers (with 26 CPU) were used to handle the large computational requirements for this problem. The FETI Domain Decomposition Method (i.e. application of parallel computers) was used, see references [1], [2] and [3].

The whole solution time for the non-linear solution (i.e. 1.04 s) was divided into 370 steps of variable length. The Full Newton-Raphson method was used for solving this non-linear problem. Solution of 500 Monte Carlo simulations (calculated simultaneously on four different parallel computers with 26 CPU) takes 70.4 hours.

4. Results and Stochastic Evaluation

Figures 8 to 9 show the equivalent stress (i.e. σ_{HMH} distributions) at some selected time t of the solution calculated for one of the chosen 500 Monte Carlo simulations (i.e. for one situation when the material of the ore is described by values $R_p = 12$ MPa, $R_m = 13.5$ MPa, $E = 20000$ MPa and $\mu = 0.2$). The movement of the bit and also the subsequent disintegration of the ore caused by the cutting are shown.

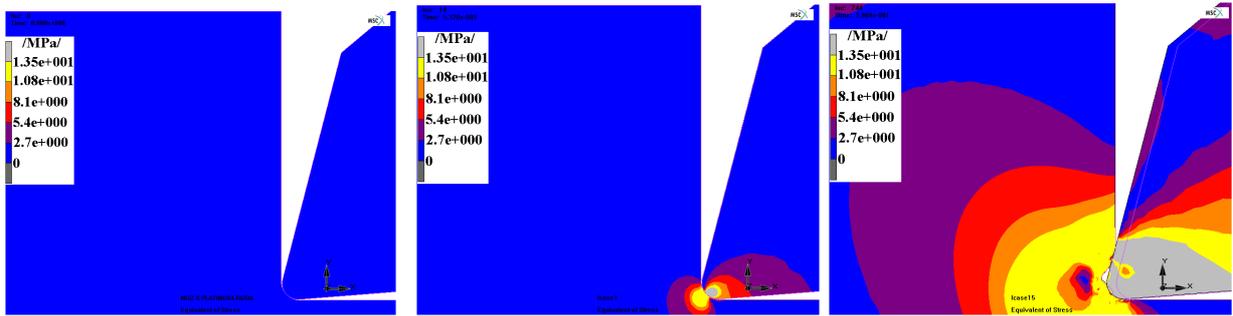


Figure 8: FEM Results ($t = 0$ s, $t = 0.00532$ s, $t = 0.1208$ s, $t = 0.2909$ s).

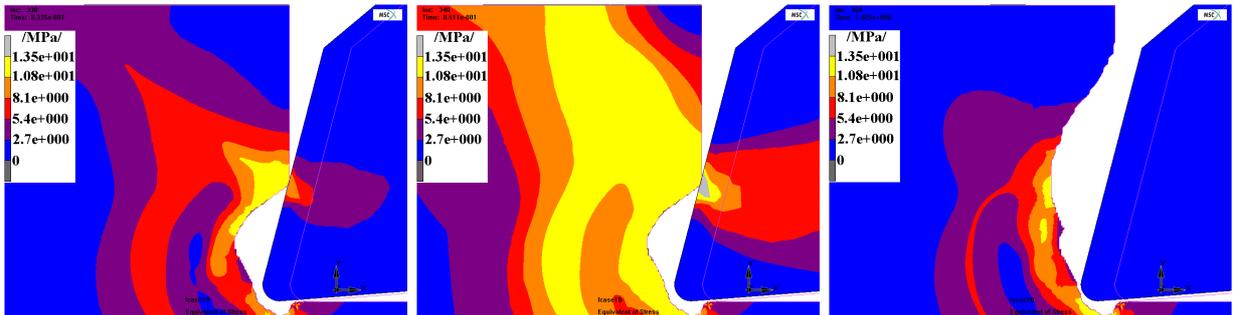


Figure 9: FEM Results ($t = 0.8335$ s, $t = 0.8511$ s, $t = 1.026$ s).

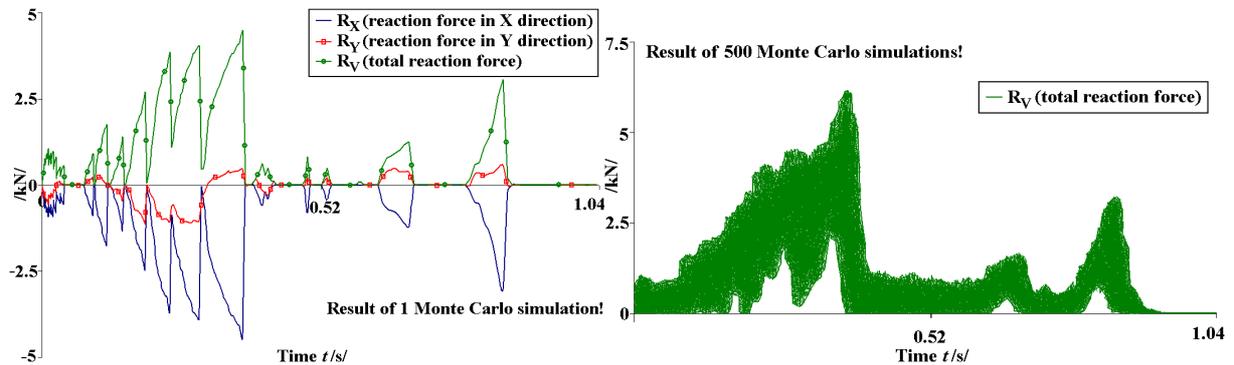


Figure 10: Reaction Forces in the Bit - SBRA-FEM Results (Results of one Monte Carlo Simulations and Results of 500 Monte Carlo simulations).

From the FEM results, the reaction forces R_X , R_Y and the total reaction force $R_V = \sqrt{R_X^2 + R_Y^2}$ can be calculated. These forces act in the bit, see Figure 10a. Figure 10a is

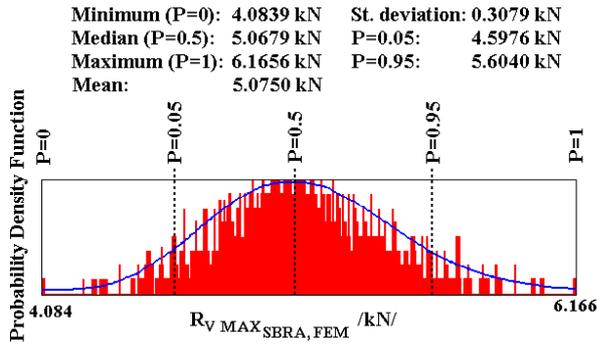


Figure 11: Maximum Total Reaction Forces in the Bit (SBRA-FEM Results of 500 Monte Carlo Simulations) and their Evaluation.

calculated for one simulation (i.e. situation when the material of the ore is described by values $R_p = 12 \text{ MPa}$, $R_m = 13.5 \text{ MPa}$, $E = 20000 \text{ MPa}$ and $\mu = 0.2$). A distribution of the total reaction forces acquired from 500 Monte Carlo simulations (i.e. stochastic result) is shown in Figure 10b.

The maximum total reaction force (acquired from 500 Monte Carlo simulation) is given by the histogram

$$R_{V \text{ MAX}_{\text{SBRA, FEM}}} = 5068^{+1098}_{-984} \text{ N}, \quad \text{see}$$

Figure 11.

5. Comparison between Stochastic Simulations and Experimental Measurements and Proposition of Fully Probabilistic Assessment

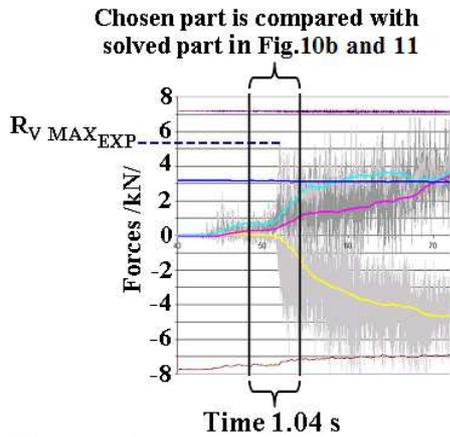


Figure 12: Experimental Measurement, compared with the SBRA-FEM Simulations.

The calculated maximum forces (i.e. SBRA-FEM solutions, see Figure 10b and 11) can be compared with the experimental measurements (i.e. compared with a part of Figure 12), see also references [1] and [4].

The evaluation of one force measurement (Figure 12) shows that the maximum force is $R_{\text{MAX}_{\text{EXP}}} = 5280 \text{ N}$. Hence, the relative error calculated for the acquired median value $R_{\text{MAX}_{\text{SBRA, FEM}} - \text{MED}} = 5068 \text{ N}$, see Figure 12, is:

$$\Delta_{R_{\text{MAX}}} = \frac{R_{\text{MAX}_{\text{EXP}}} - R_{V \text{ MAX}_{\text{SBRA, FEM}} - \text{MED}}}{0.01 \times R_{\text{MAX}_{\text{EXP}}}} = 4.02 \%$$

The error of 4.02% is acceptable. However, the experimental results also have large variability due to the anisotropic and stochastic properties of the material and due to the large variability of the reaction forces.

Reliability function RF , see references [1] and [4], can be defined by: $RF = R_{V \text{ MAX}_{\text{ALLOWABLE}}} - R_{V \text{ MAX}_{\text{SBRA, FEM}}}$, where $R_{V \text{ MAX}_{\text{ALLOWABLE}}}$ is the allowable reaction force in the cutting bit, which can be acquired from the real capacity of the whole cutter-loader system in the mine. If situations when $RF \leq 0$ occur, then the cutter-loader system is overloaded. Else if $RF > 0$, then safe situations of loading occurs. Hence, fully probabilistic assessment can be calculated by comparing of probabilities: $P(RF \leq 0) \leq P_{\text{ALLOWABLE}}$, where $P_{\text{ALLOWABLE}}$ is the acceptable probability of overloading of the cutting-loader system. This overloading sometimes really occurs in the mine. Value of $P_{\text{ALLOWABLE}}$ can be given by chosen performance requirements of the client (i.e. investor).

6. Conclusions

This paper combines the SBRA (Simulation Based Reliability Assessment) Method and FEM as a suitable tool for simulating the hard rock (ore) disintegration process. All basic

factors have been explained (i.e. 2D boundary conditions, material nonlinearities, mechanical contacts and friction between the cutting bit and the ore, the methodology for deactivating the finite elements during the ore disintegration process, application of parallel computers). The use of finite element deactivation during the ore disintegration process (as a way of expanding the crack) is a modern and innovative way of solving problems of this type. The error of the SBRA-FEM results (i.e. in comparison with the experiments) is acceptable. Hence, SBRA and FEM can be a useful tool for simulating the ore disintegration process.

Because the real material of the ore (i.e. yield limit, fracture limit, Young's modulus, Poisson's ratio etc.) is extremely variable, stochastic theory and probability theory were applied (i.e. application of the SBRA Method). The SBRA Method, which is based on Monte Carlo simulations, can include all stochastic (real) inputs and then all results are also of stochastic quantities. However, for better application of the SBRA method (for simulating this large problem of mechanics), it is necessary to use superfast parallel computers. Instead of 500 Monte Carlo simulations (wall time cca 70.4 hours, as presented in this article), it is necessary to calculate $>10^4$ simulations (wall time cca 58 days or more). Our department will be able to make these calculations when new and faster parallel computers become available.

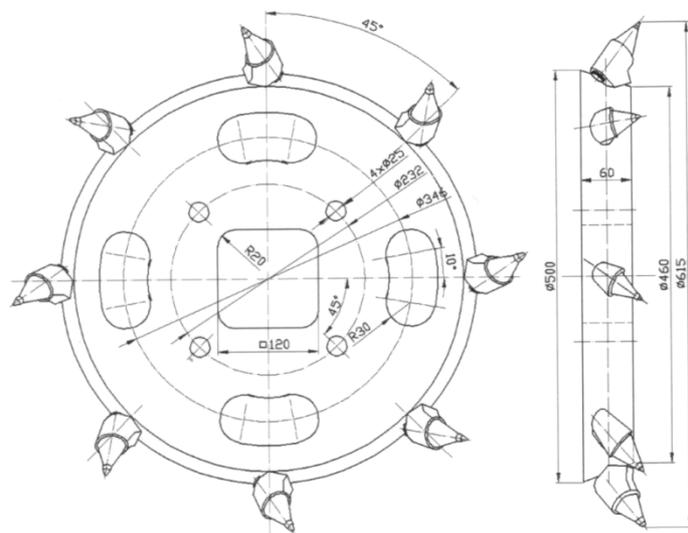


Figure 13: Final Shape of Excavation Tool for Platinum Ore Disintegration Process.

Hence, the fully probabilistic assessment was proposed according to the acceptable probability of overloading of the whole cutting-loader system.

All the results presented here were applied for optimizing and redesigning of the cutting bit (excavation tool), see Figure 13 and reference [5].

In the future, 3D FE models (instead of 2D plane strain formulation) will be applied for greater accuracy.

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References

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